

Overland Flow Study Report

**265-267 King Georges Road,
Roselands**

Prepared for Evolve Pacific Developments / 26 July 2016

161087 PA

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Taylor Thomson Whitting Pty. Ltd. (TTW) has been engaged by Evolve Pacific Developments to undertake a flood study for the proposed development at 265-267 King Georges Road, Roselands NSW. The purpose of the study is to quantify the upstream overland flow for the 100 year Annual Recurrence Interval (ARI) storm event and the Probable Maximum Precipitation (PMP) storm event, and determine the extent of the flow conveyance through the development site.

The proposed development will be situated on the proposed amalgamation of 265 and 267 King Georges Road, Roselands. The two existing dwellings are proposed to be demolished with new affordable living units to be constructed. The amalgamated site is bounded by an existing multi-residential dwelling to the north, King Georges Road to the east, and existing dwellings on its southern and western boundaries.

S.P. 5448

LOT 21
D.P. 558875
AREA 739.9m² (TITLE)

LOT 22
D.P. 558875
AREA 663.9m² (TITLE)

LOT 32
D.P. 602446

LOT 31
D.P. 602446

RIGHT OF CARRIAGEWAY & EASEMENT
TO DRAIN SEWAGE (3.31 METER)

KING

GEORGES

ROAD

The proposed development consists of two new multi residential dwellings with a centralised access pathway. A new car park is proposed to be provided at the building frontage to King Georges Road to service 6 cars, inclusive of 3 disabled spots. A communal landscaping area is proposed at the rear of the property.



1.2 Referenced Documents

This report, and the findings within, has been prepared upon reviewing the following documents:

- City of Canterbury-Bankstown Development Control Plan 2012 (CCB DCP) – Part 6.4 Developments Engineering, Flooding and Stormwater
- Australian Rainfall and Runoff 1987 (AR&R)
- Commonwealth Bureau of Meteorology (BoM)
- Map images courtesy of Nearmaps
- NSW LiDAR Survey Data 2013
- NSW Flood Development Manual
- Existing land survey plan prepared by Lawrence Group
- Architectural plans prepared by Sissons Architects

2.0 Upstream Catchment

The upstream overland flow catchment has been sized using both visual inspection and using the NSW Lidar survey. The upstream catchment further divides into sub-catchments, whereby only a portion affects the development site. Refer Figure 3 for catchment plan.



Figure 3 - Upstream Catchment Plan

Legend

Catchment A = Blue
Catchment B = Yellow
Catchment C = Green

As suggested above, Catchment C is the portion of the upstream catchment falling towards the site, with Catchment A and B falling and draining away from the site.

- Catchment A has a main overland flow route down the southern side of Penshurst Street. The crown of Penshurst Street cuts off and redirects the overland flow traversing down through the properties and Beggs Street towards King Georges Road.
- Catchment B utilises the northern side of Penshurst Street and Georges Crescent and the main overland flow route. Flow then traverses through the downstream properties at the end of Georges Crescent adjacent to the development site.
- Overland flow from Catchment C sheets between the properties upstream of the development site and continues similarly through and downstream.

Utilising an Intensity Frequency Distribution (IFD) table generated and provided by BoM, the information was relayed into DRAINS to quantify the overland flows generated by the upstream catchments. The following figures demonstrate the model setup in DRAINS and the results for the 100 year ARI and PMP storm events.

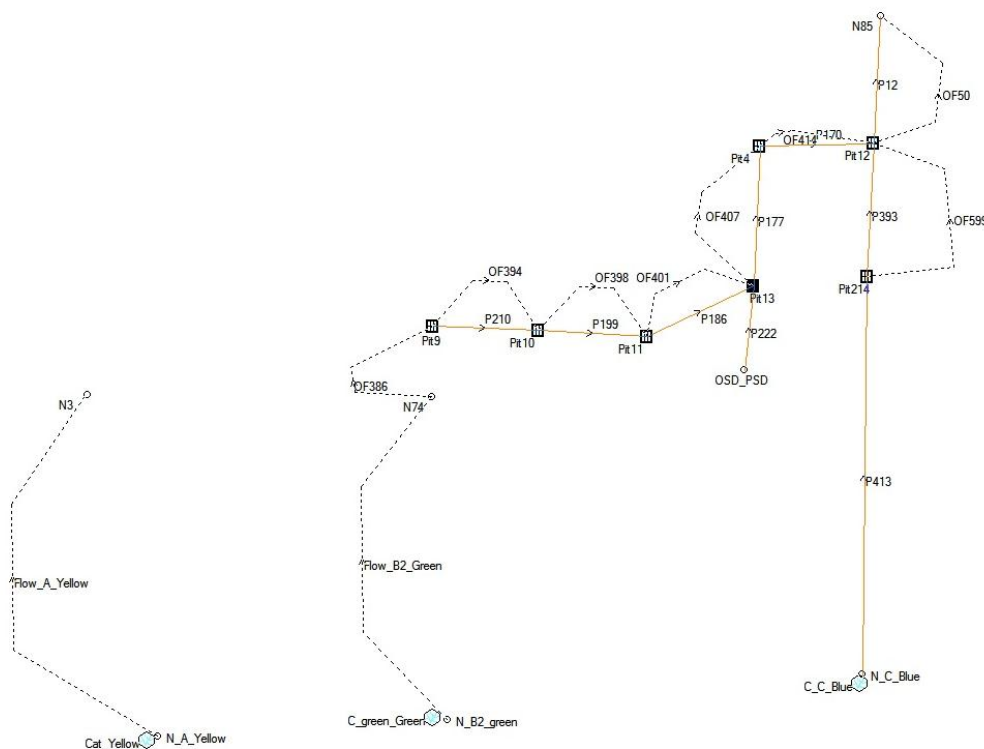


Figure 4 - DRAINS Model Setup

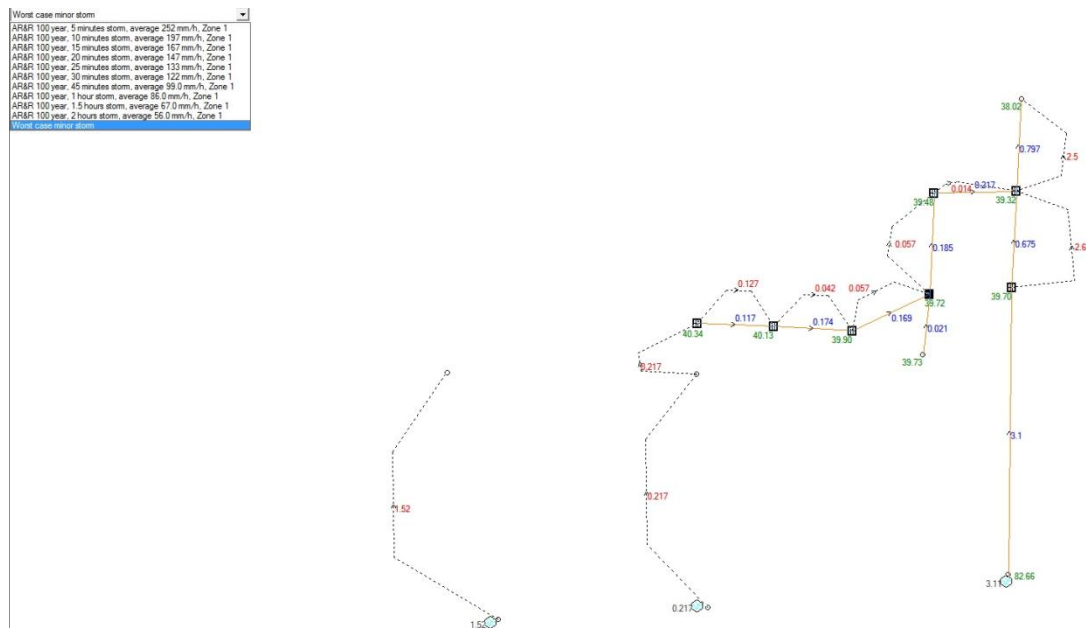


Figure 5 – 100 year ARI storm event

The critical storm for the 100 year ARI event was 20 minutes.

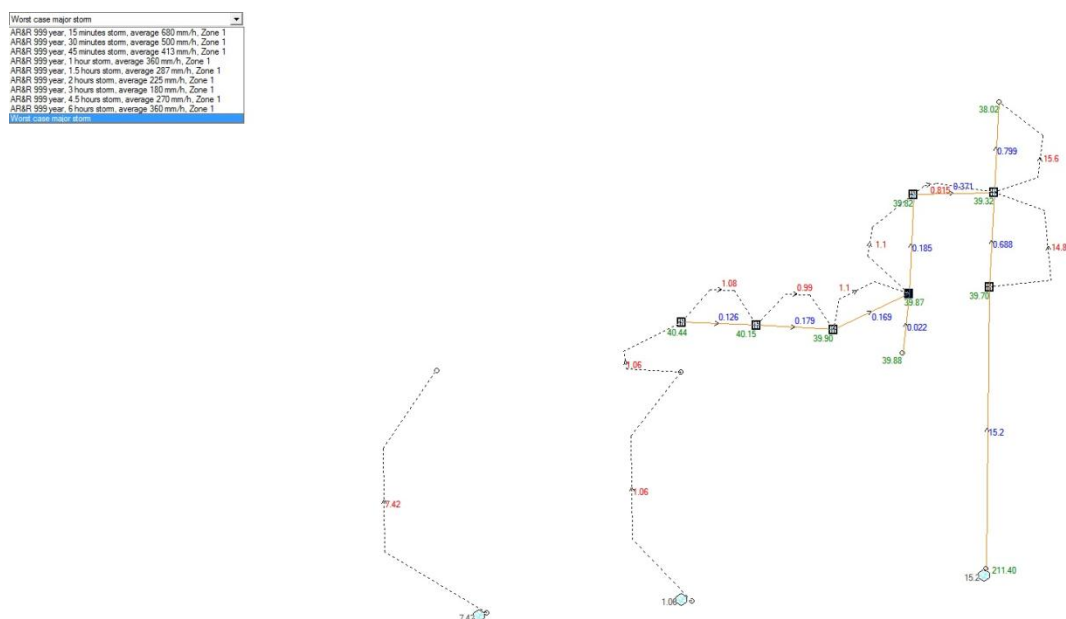


Figure 6 - PMP storm event

3.0 Overland Flow Modelling

The flows obtained in the DRAINS were further modelled in HEC-RAS to determine the channelized water levels. Two HEC-RAS models were created to analyse the upstream overland flows:

- Catchment B model – demonstrates the likely water levels from the flow generated by Catchment B. The 100 year ARI and PMP storm events were analysed with results demonstrating that the development site is not subjected to overland flows from Catchment B. Existing buildings, fencing and retaining walls in the adjacent

properties to the development site have been incorporated into the model to demonstrate they prevent the site being subjected to the overland flow.

- Catchment C model - demonstrates the proposed landscape channel within the development site along its southern boundary to intercept the overland flow from the upstream properties for conveyance towards King Georges Road. This alters from the existing scenario and relieves the downstream properties of overland flow inundation. The channel is sized to cater for the PMP storm event.

No existing in ground stormwater infrastructure was included in the above model for a conservative approach. Refer Appendix A for HEC-RAS model and extent of overland model plan.

As Catchment A is directed towards King Georges Road further upstream, the overland flow route was analysed as a typical road section in DRAINS to obtain flow depth to determine if flow inundates the development site on its eastern boundary. The 100 year ARI and PMP storm events were analysed with the 100 year ARI event demonstrated to be safely contained within the road reserve. The PMP storm event flow inundates the site only at the driveway and exits as per the proposed overland flow path within the site. Refer to the following figures for King Georges Road section analysis.

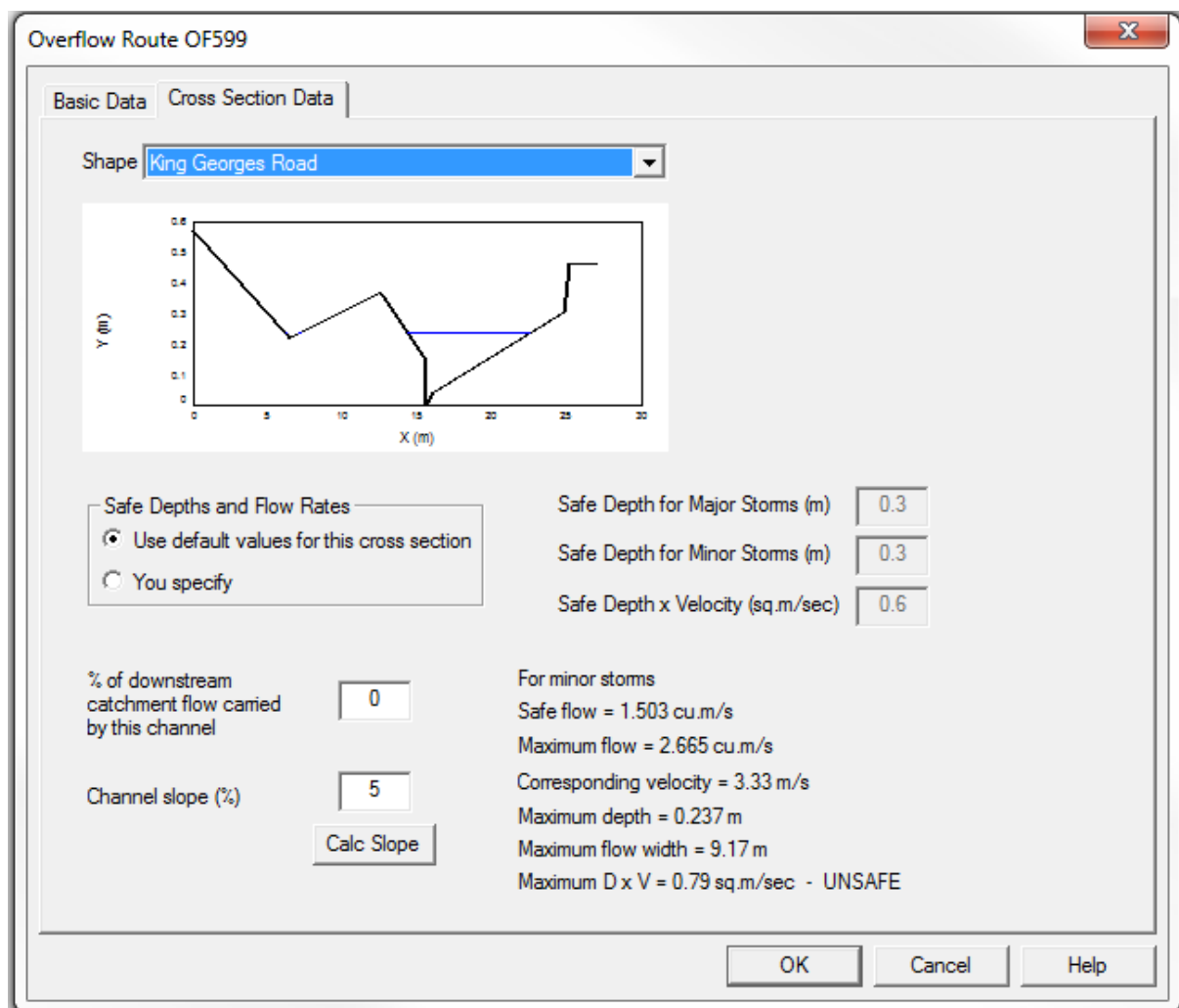


Figure 7 - King Georges Road typical section analysis in DRAINS for 100 year ARI storm event

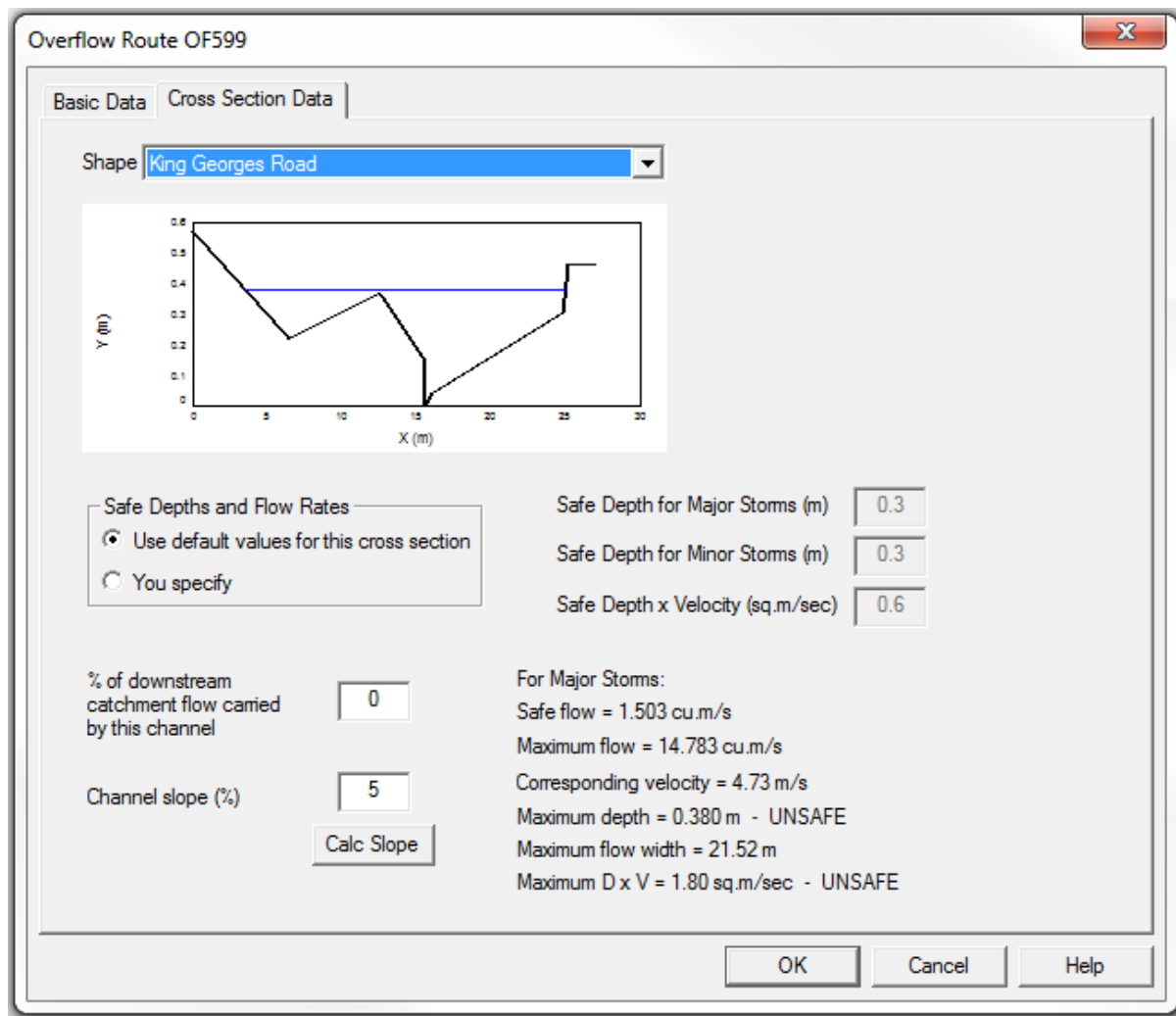


Figure 8 - King Georges Road typical section analysis in DRAINS for PMP storm event

4.0 Flood Evacuation Strategy

In accordance with NSW's Flood Development Manual, along with industry practice, an evacuation strategy is to be set in place to cater for all storms up to and including the PMP event. TTW's analysis demonstrates the overland flow paths pertaining to the site from the upstream catchments do not impose an immediate threat to the residents. The proposed finished floor levels are set above the PMP storm event overland flow levels, thus residents will not be required to be evacuated as part of the strategy and can stay put.

5.0 Summary

From the results, we summarise and recommend the following:

- The Finished Floor Levels (FFL) of the units to be at RL 40.20 Australian Height Datum (AHD);
- A bund or wall to be provided at the upstream end of the proposed landscape channel to ensure the upstream overland flow is capture and conveyed through the channel;
- A piped system to be provided within the proposed landscaped channel to capture the smaller, more frequent storm events;
- All openings including windows, vents, etc. adjacent to the channel to be set at a minimum level of RL 41.00 AHD;
- Southern building adjacent to proposed channel to be constructed with water resistant materials to a minimum level of RL41.00 AHD;
- No concentrate number of small shrubs to be provided to the landscaped channel, only long stemmed (trunk) planting;
- A reduced overland flow quantity inundating downstream proposed as overland flow is now directed towards King Georges Road.

The above recommendations are outlined on the plan affixed in Appendix B

Prepared by
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Chris Veleski
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Authorised By
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Nemesio Biason
Associate

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Appendix A

Overland Flow Results

1. HEC-RAS Model and Extent of Overland Flow Plan

2. Longitudinal Section of Catchment B Model

3. Cross Sections of Catchment B Model

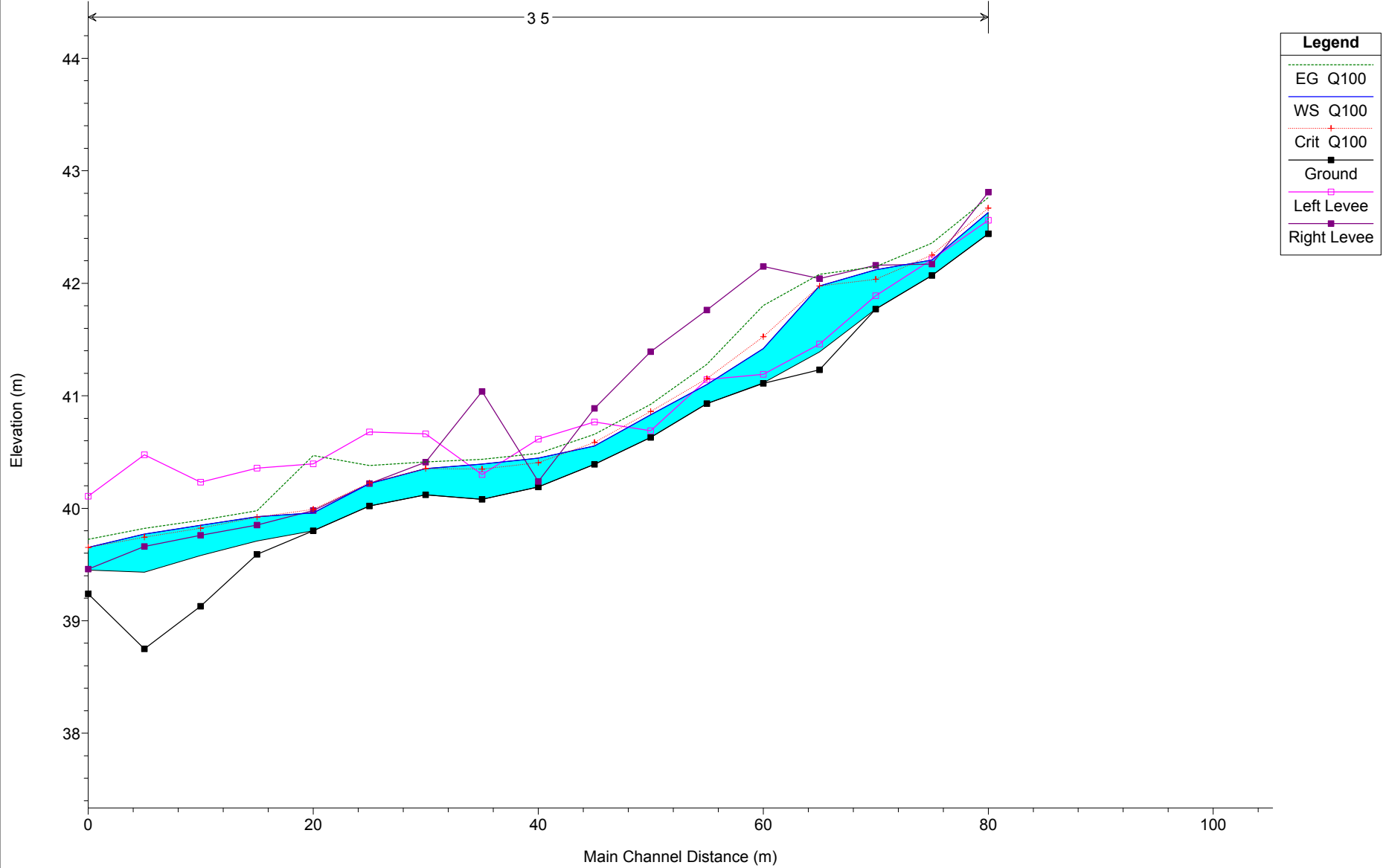
4. Velocities of Catchment B Model

5. Longitudinal Section of Catchment C Model (Proposed Channel)

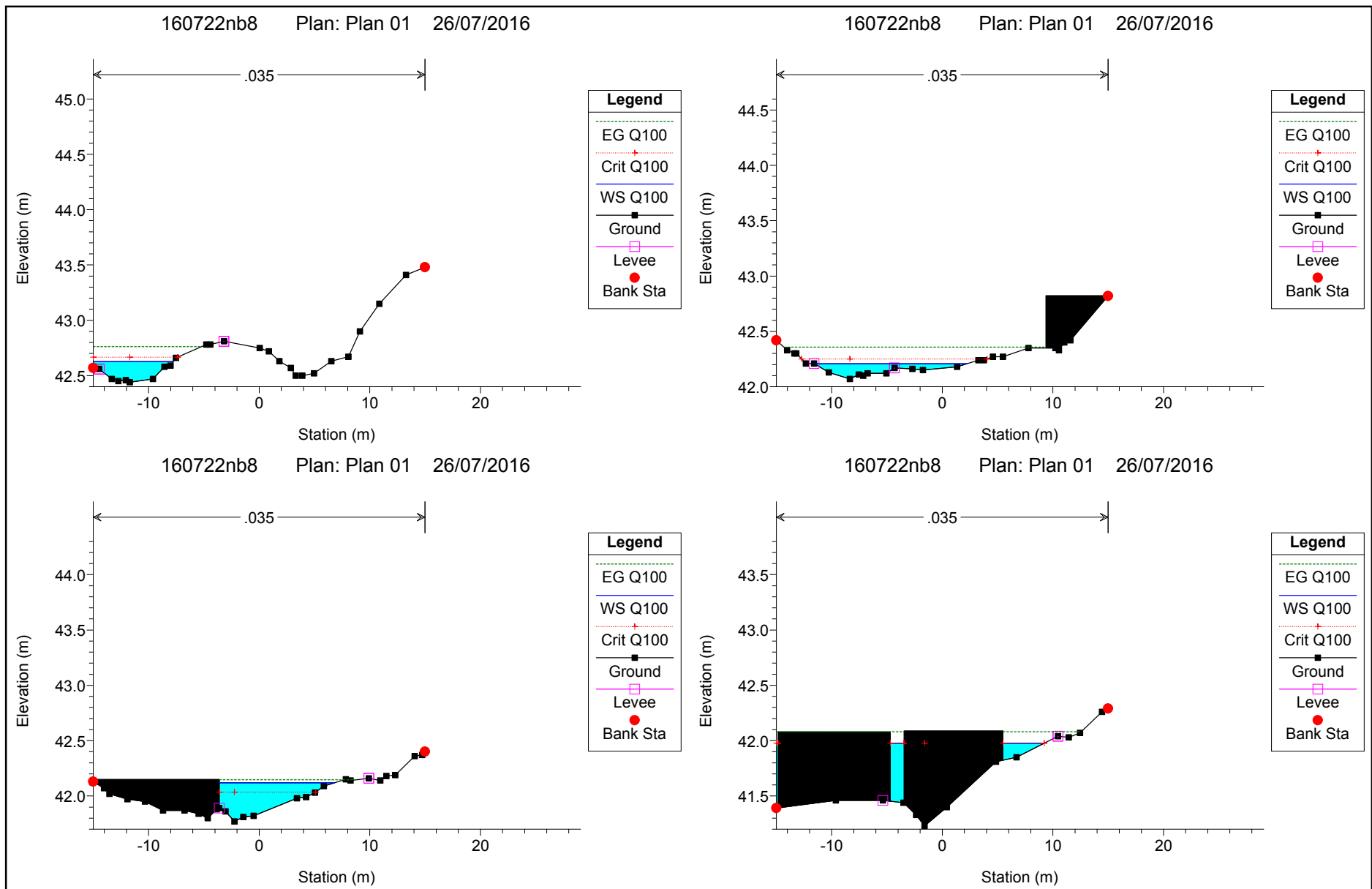
6. Cross Sections of Catchment C Model (Proposed Channel)

7. Velocities of Catchment C Model (Proposed Channel)

160722nb8 Plan: Plan 01 26/07/2016



1 cm Horiz. = 5 m 1 cm Vert. = 0.5 m

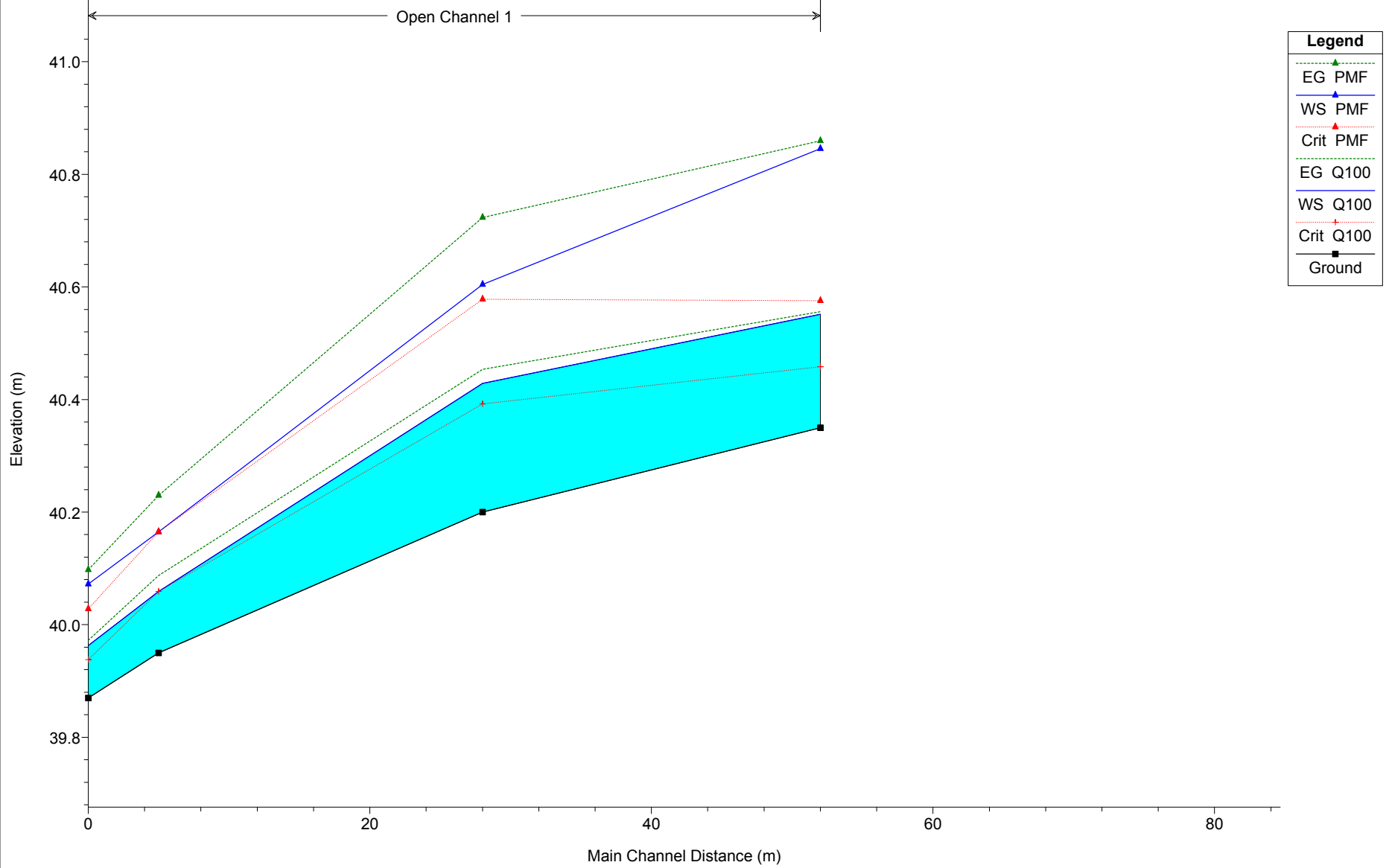


Catchment B

HEC-RAS Plan: Plan 01 River: 3 Reach: 5

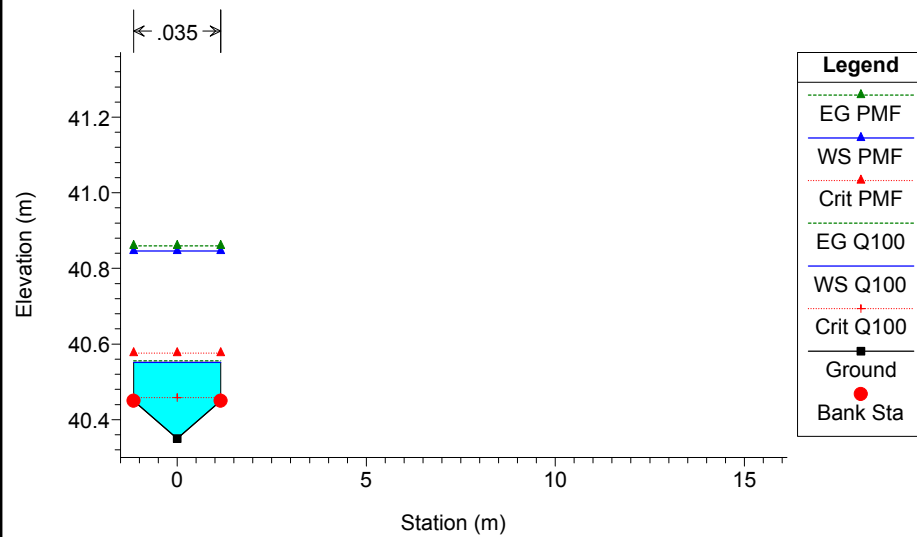
Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude #	Chl
5	85	Q100	1.52	42.44	42.63	42.67	42.76	0.050093	1.62	0.94	7.24	1.44	
5	85	QPMP	7.42	42.44	42.84	42.84	42.95	0.020558	1.45	5.11	23.85	1	
5	80	Q100	1.52	42.07	42.21	42.25	42.36	0.140866	1.72	0.88	13.77	2.17	
5	80	QPMP	7.42	42.07	42.31	42.42	42.7	0.141223	2.78	2.67	20.27	2.44	
5	75	Q100	1.52	41.77	42.12	42.03	42.15	0.00607	0.74	2.05	10.41	0.53	
5	75	QPMP	7.42	41.77	42.32	42.26	42.38	0.008518	1.04	7.17	28.69	0.66	
5	70	Q100	1.52	41.39	41.98	41.98	42.08	0.033498	1.43	1.07	5.1	1	
5	70	QPMP	7.42	41.39	42.22	42.22	42.31	0.023154	1.34	5.52	28.99	0.98	
5	65	Q100	1.52	41.11	41.42	41.53	41.8	0.088333	2.74	0.55	1.85	1.6	
5	65	QPMP	7.42	41.11	41.77	41.87	42.09	0.075592	2.52	2.95	13.83	1.74	
5	60	Q100	1.52	40.93	41.1	41.15	41.28	0.096779	1.88	0.81	8.25	1.91	
5	60	QPMP	7.42	40.93	41.27	41.44	41.7	0.081767	2.9	2.56	11.87	1.99	
5	55	Q100	1.52	40.63	40.83	40.86	40.92	0.049102	1.36	1.12	11.28	1.37	
5	55	QPMP	7.42	40.63	40.96	41.05	41.26	0.076519	2.42	3.06	18.04	1.88	
5	50	Q100	1.52	40.39	40.55	40.58	40.66	0.056766	1.43	1.06	10.94	1.47	
5	50	QPMP	7.42	40.39	40.73	40.82	40.97	0.043	2.17	3.42	15.43	1.47	
5	45	Q100	1.52	40.19	40.44	40.4	40.49	0.011038	0.92	1.65	9.66	0.71	
5	45	QPMP	7.42	40.19	40.79	40.67	40.87	0.006129	1.23	6.06	14.7	0.61	
5	40	Q100	1.52	40.08	40.39	40.35	40.44	0.009739	0.93	1.64	8.53	0.68	
5	40	QPMP	7.42	40.08	40.63	40.63	40.81	0.017324	1.88	3.94	10.89	0.99	

5	35 Q100	1.52	40.12	40.35	40.35	40.41	0.003112	1.08	1.41	11.21	0.97
5	35 QPMP	7.42	40.12	40.56	40.56	40.69	0.002529	1.6	4.65	17.34	0.98
5	30 Q100	1.52	40.02	40.22	40.23	40.38	0.009381	1.77	0.86	7.38	1.66
5	30 QPMP	7.42	40.02	40.29	40.39	40.64	0.014025	2.65	2.8	17.65	2.13
5	25 Q100	1.52	39.8	39.96	39.99	40.47	0.496882	3.16	0.48	7.72	4.05
5	25 QPMP	7.42	39.8	40.04	40.16	40.47	0.124497	2.66	2.62	17.65	2.31
5	20 Q100	1.52	39.71	39.93	39.92	39.98	0.020129	1.01	1.51	12.05	0.91
5	20 QPMP	7.42	39.71	40.04	40.14	40.35	0.056307	2.46	3.02	13.53	1.66
5	15 Q100	1.52	39.58	39.85	39.82	39.89	0.013611	0.93	1.64	10.88	0.76
5	15 QPMP	7.42	39.58	40.03	40.06	40.17	0.030239	1.63	4.55	23.73	1.19
5	10 Q100	1.52	39.43	39.77	39.74	39.82	0.014578	0.99	1.53	9.62	0.79
5	10 QPMP	7.42	39.43	40.01	39.95	40.08	0.009391	1.14	6.51	24.01	0.7
5	5 Q100	1.52	39.45	39.65	39.65	39.72	0.026383	1.18	1.29	9.83	1.04
5	5 QPMP	7.42	39.45	39.88	39.88	40.01	0.020488	1.57	4.73	19.45	1.02

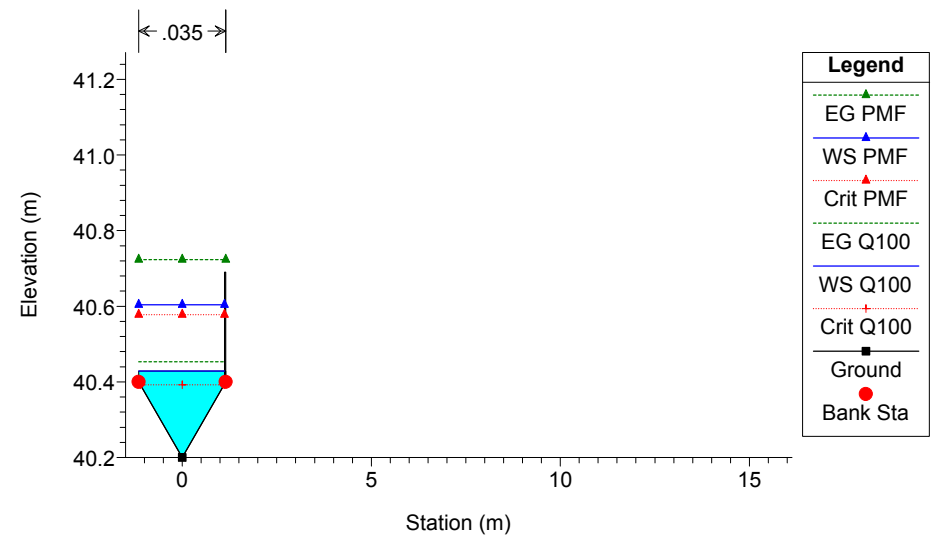


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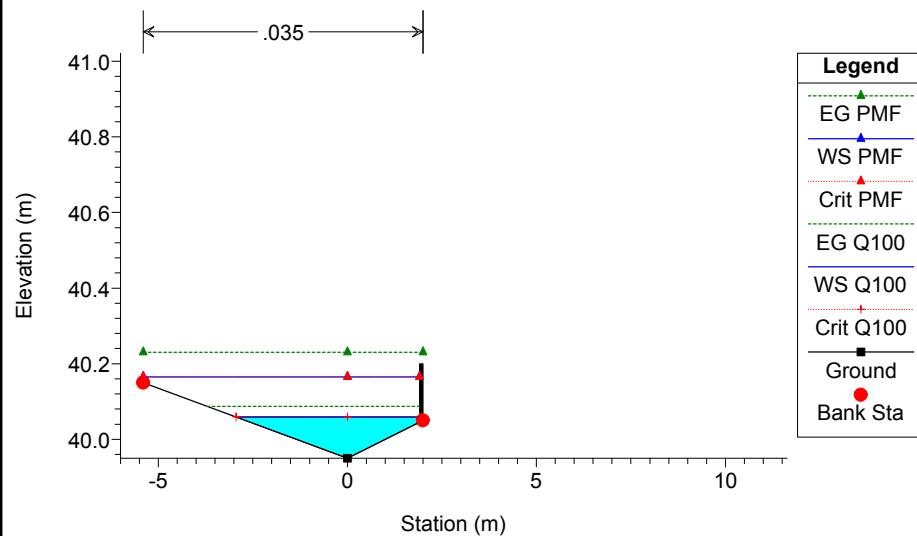
Proposed Channel_nb Plan: Plan 03 26/07/2016



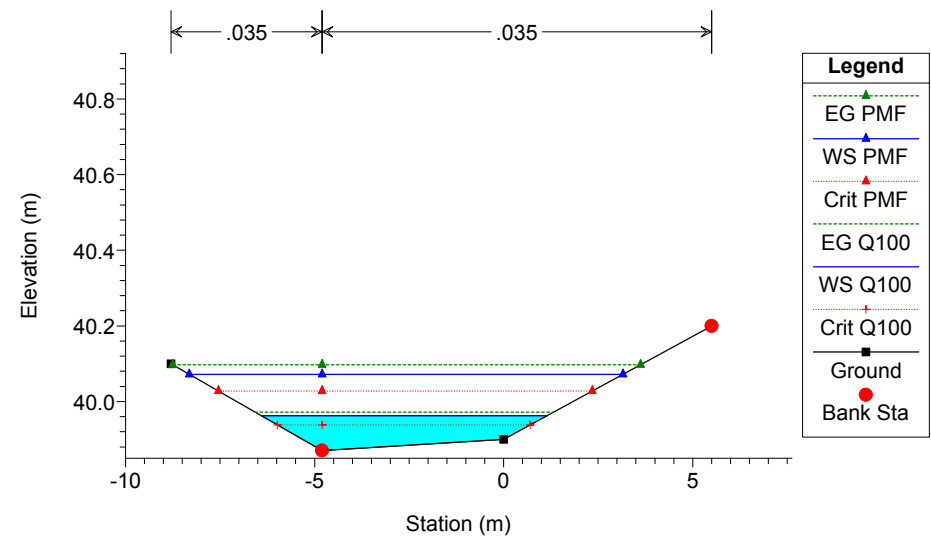
Proposed Channel_nb Plan: Plan 03 26/07/2016



Proposed Channel_nb Plan: Plan 03 26/07/2016



Proposed Channel_nb Plan: Plan 03 26/07/2016



1 cm Horiz. = 2 m 1 cm Vert. = 0.2 m

Catchment C

HEC-RAS Plan: Plan 03 River: Open Channel Reach: 1

Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude #	Chl
1	52	Q100	0.1	40.35	40.55	40.46	40.56	0.001387	0.29	0.36	2.3	0.23	
1	52	QPMP	0.53	40.35	40.85	40.58	40.86	0.001411	0.51	1.03	2.3	0.25	
1	28	Q100	0.21	40.2	40.42	40.4	40.45	0.011569	0.74	0.28	2.27	0.68	
1	28	QPMP	1.06	40.2	40.6	40.58	40.72	0.017707	1.53	0.69	2.27	0.88	
1	5	Q100	0.21	39.95	40.06	40.06	40.09	0.023396	0.67	0.31	5.01	0.87	
1	5	QPMP	1.06	39.95	40.16	40.16	40.23	0.024724	1.13	0.94	7.31	1.01	
1	0	Q100	0.21	39.87	39.96	39.94	39.97	0.008503	0.44	0.48	7.56	0.54	
1	0	QPMP	1.06	39.87	40.07	40.02	40.1	0.008515	0.73	1.52	11.46	0.61	

Appendix B

Flood Mitigation and Protection Plan

FLOOD MITIGATION AND PROTECTION PLAN

- NO LANDSCAPING MOUND
- NO WALLS
- NO STRUCTURES BLOCKING THE OVERLAND FLOWPATH

100mm heelsafe grated drain shown as (typ)

OVERLAND FLOWPATH

LANDSCAPING MOUND TO 41.0 RL

LIGHT LANDSCAPING ONLY

LANDSCAPING TO BE LIMITED TO LONG STEM PLANTING

FLOODPROOF TO 41.0 RL.

FLOODPROOF TO 41.0 RL

TOP OF WALL VARIES TO MATCH EXISTING SOUTHERN NEIGHBOUR'S LEVELS

SECTION ② - NOT TO SCALE

SECTION ③ - NOT TO SCALE

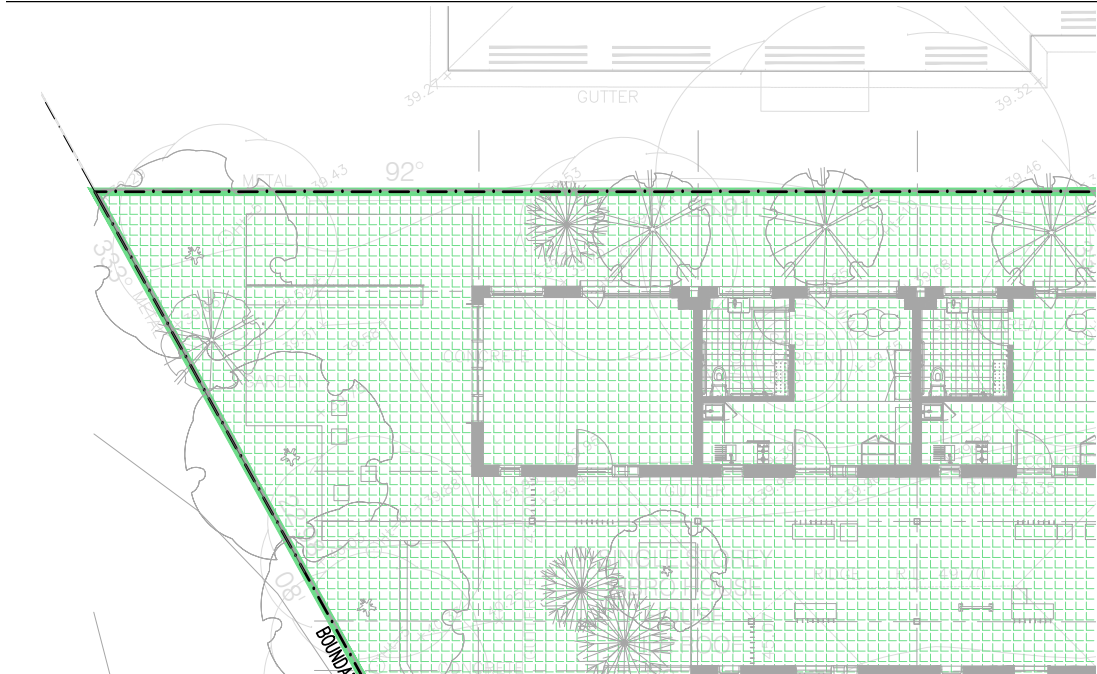
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Appendix C

Revised Concept Stormwater Management Drawings

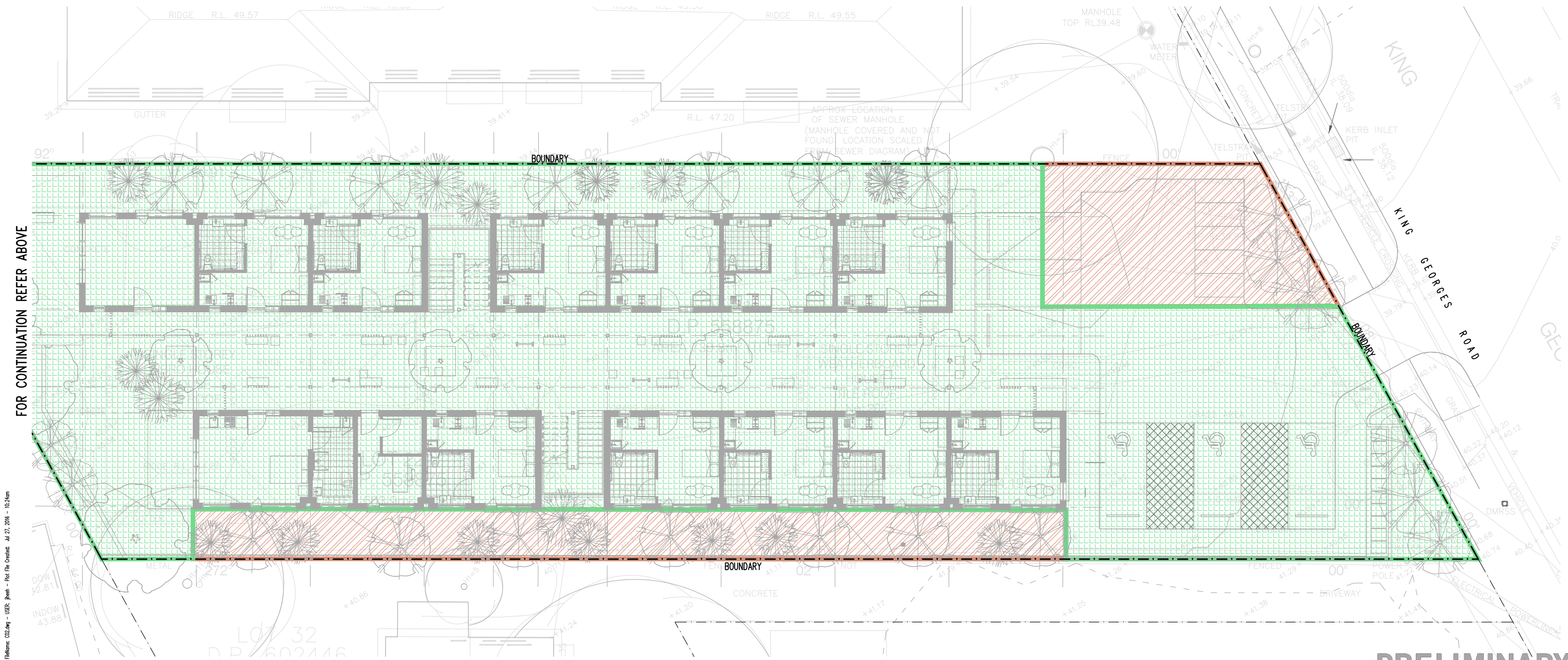
PRELIMINARY



FOR CONTINUATION REFER BELOW

Catchment Notes

Total Site Area = 1410.2m²
Catchment draining to Onsite Detention = 1203.4m² (85.3%)
Catchment bypassing Onsite Detention = 206.8m² (14.7%)
Permissible Site Discharge Rate: 150L/s/ha
Permissible Site Discharge = 0.14102x150 = 21.153 L/s
DRAINS was utilised to size Site Storage Requirement to meet permissible site discharge. Refer C04 for OSD detail.



FOR CONTINUATION REFER ABOVE

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P1	ISSUED FOR DEVELOPMENT APPROVAL	CV	CV 29.04.16
Rev	Description	Eng	Draft Date
Rev	Description	Eng	Draft Date

Architect
SISSONS ARCHITECTS PTY. LTD.
Studio 5, 81 Alexander Street
Crows Nest, NSW, 2065
t. (02) 9460 8002

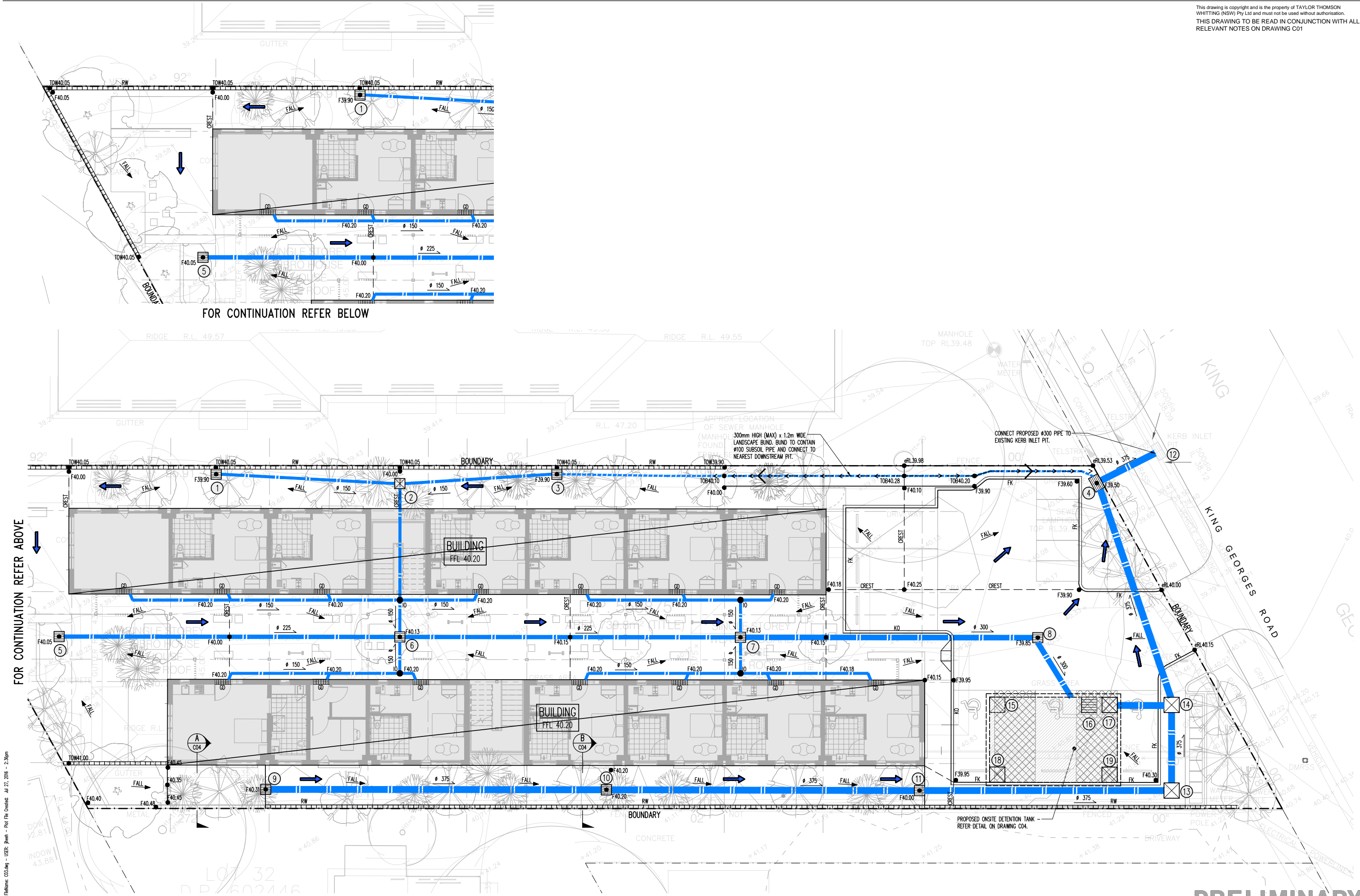
TTW Taylor Thomson Whitting
612 9439 7288 | 48 Chandos Street St Leonards NSW 2065

Project
265 / 267
KING GEORGES ROAD,
ROSELANDS

Sheet Subject
CATCHMENT PLAN

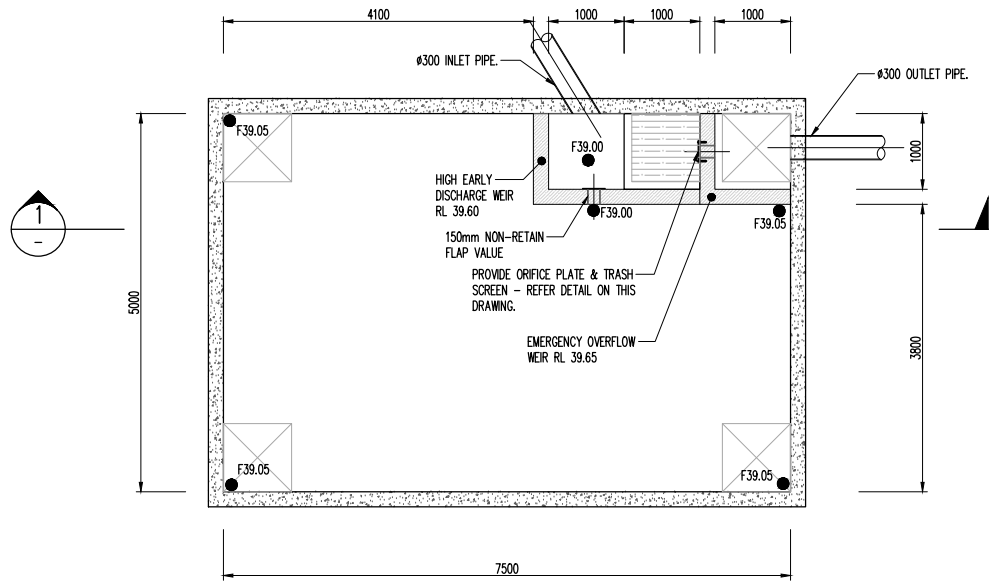
PRELIMINARY

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Revision
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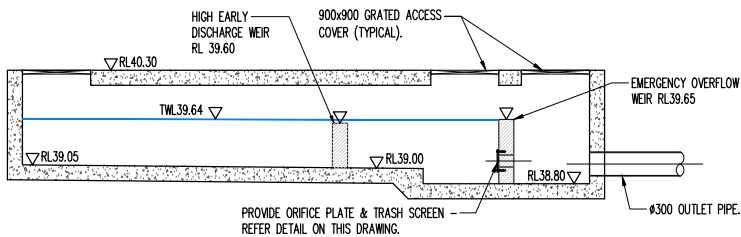


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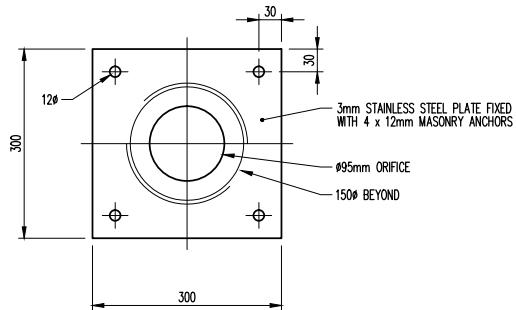
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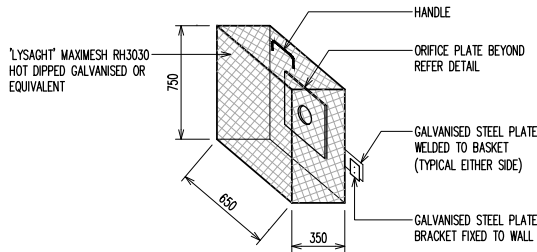
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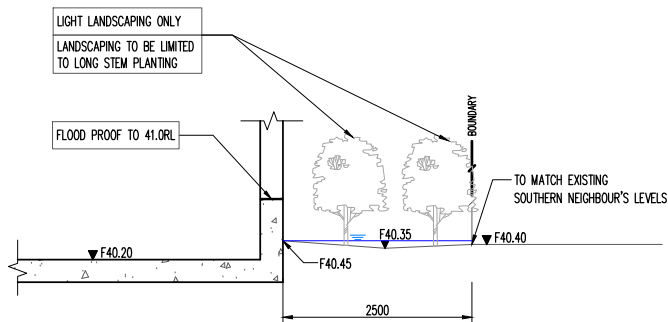
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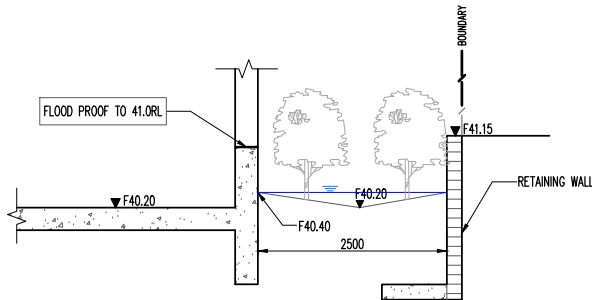
ORIFICE PLATE DETAIL
NTS



TRASH SCREEN
SCALE 1:10



SECTION A
SCALE 1:50



SECTION B
SCALE 1:50

Filename: C01.dwg - User: jwh - Plot File Created: Jul 27, 2016 - 2:39pm

A1 1 2 3 4 5 6 7 8 9 10

			Architect			Project			Sheet Subject		
			SISSONS ARCHITECTS PTY. LTD.			265 / 267 KING GEORGES ROAD, ROSELANDS			SITEWORKS & STORMWATER PLAN		
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P1	ISSUED FOR DEVELOPMENT APPROVAL	CV	CV	29.04.16							
Rev	Description	Eng	Draft	Date	Rev	Description	Eng	Draft	Date	Rev	Description

PRELIMINARY